

FUNFI-IT - Italian Meeting on Fusion Neutrons for Fission

Breeding Blanket concepts for the EU-DEMO Fusion Power Plant

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) Breeding Blanket R&D Programme: Background

- Breeding blanket technology is crucial for the development of fusion power, but its maturity is currently very poor.
 - Heat removal for electrical production: (~300-500 MWe) predictably and safely, with minimal environmental impact
 - use Reduced Activation Ferritic-Martensitic 'RAFM' steel \rightarrow EUROFER
 - minimization of tritium permeation, dust and corrosion products generation
 - Breed tritium: "a 2 GW fusion power DEMO will consume around 111 kg T/FPY, and this clearly underscore the indispensable requirement to achieve Tself-sufficiency"
 - Radiation Shielding of the Vacuum Vessel and Coils
 - Absorb plasma radiation on the first wall
 - Dose in epoxy / 10 fpys Limit: 50 MGy
 - N-heating Limit: ~444 W/m³ (TF cond.)
 - The main BB Loads and boundary conditions are:
 - Inertial (dead weight and earthquake)
 - Thermal (nuclear heating and heat fluxes)
 - Pressure and Electromagnetic loads
 - Material damage



M. Kovari et al, (2018) Tritium resources available for fusion reactors, Nuclear Fusion, 58, 026010, DOI: 10.1088/1741-4326/aa9d25





Why Tritium?

The D-T reaction is the easiest and most promising solution to earth-based fusion

$${}_{1}^{2}D + {}_{1}^{3}T \rightarrow {}_{2}^{4}He + {}_{0}^{1}n \quad (Q_{DT} = 17.59MeV)$$

- Exothermic
- Good cross section
- Good energy release
- Deuterium is largely available

➤ ~154 ppm of D in H

- Tritium can be **bred** from Lithium
- Lithium is abundant on the Earth surface and in seawater 230 billion tons 0.1-0.2 ppm

$${}^{2}_{1}D + {}^{2}_{1}D \rightarrow \begin{cases} {}^{3}_{2}He + {}^{1}_{0}n & (Q_{DD} = 3.27MeV) \\ {}^{3}_{1}T + {}^{1}_{1}p & (Q_{DD} = 4.03MeV) \end{cases}$$
$${}^{1}_{1}p + {}^{2}_{1}D \rightarrow {}^{3}_{2}He + \gamma & (Q_{pT} = 5.59MeV) \\ {}^{2}_{1}D + {}^{3}_{2}He \rightarrow {}^{4}_{2}He + {}^{1}_{1}p & (Q_{DHe} = 18.35MeV) \end{cases}$$

 $E_n = 14.1 \text{ MeV}$ $E_\alpha = 3.5 \text{ MeV}$

n + 14.1 MeV





Tritium production in reactor: Li reactions

 ${}_{3}^{6}Li + n^{0} \rightarrow {}_{2}^{4}He + {}_{1}^{3}H + 4.78 MeV$

 ${}^{7}_{3}Li + n^{0} \rightarrow {}^{4}_{2}He + {}^{3}_{1}H + n^{0} - 2.47 MeV$

- The ⁶Li reaction has a very high cross section especially in the low-energy region
- The ⁷Li reaction works with the high energy neutrons. It produce an additional n that is available for a successive reaction
- Natural mixture: ⁷Li 92.5 % at., only 7.5 % ⁶Li
 - > About 10¹¹ kg Lithium in landmass
 - > About 10¹⁴ kg Lithium in oceans





Neutron multiplication

Required (n,2n) reactions with high σ in energy range up to 14MeV

- Li (nat.):
 - > sufficient, but only with very low n-absorber materials
 - strong reaction with water and air
 - > getter for T (difficult recovery)
- Beryllium (Be)
 - > (n,2n) threshold energy ≈2 MeV
 - good moderator (shielding)
 - exothermal reaction with water > 600°C
 - > Be dust is toxic
- Lead (Pb):
 - high availability, low cost
 - can be used as coolant
 - melting point ~235°C
 - > corrosion with material (e.g. steels)
 - weight
 - activation through Po formation
 - (moderate) reaction with water

- Beryllides (TiBe₁₂, CrBe₁₂, etc.)
 - Tritium breeding ratio 1.20
 - Well developed industrial technology
 - Excellent combination of properties
 - Annual production of Be 300 t/ yr
 - Cost of Be 650 \$/kg
- Plumbides (LaPb₃, YPb₂, Zr₅Pb₃)
 - > (n,2n) threshold energy ≈7.5 MeV
 - No industrial technology
 - Properties are not well studied
 - Annual production of Pb 11 mln t/ yr
 - Cost of Pb 6 8 \$/kg





Tritium Breeding Ratio (TBR)

TBR = 1 is achieved when every fusion neutron produces a triton from lithium

TBR = <u>Tritium Bred</u> > 1 Tritium Burnt

- It has to be > 1 for reactor auto sufficiency;
- Depends on the choice of materials and geometry
- Relies in neutron multiplication and reflection
- Can be calculated using Montecarlo codes (MCNP)
- Can be validated by experiments
- Typical design targets of the global TBR are in the range of 1.05 1.15
- Whether achievable in a fusion reactor is a question of design integration...
- Multipliers need to offset absorption in all other components and materials, e.g. FW, divertor, pellet injectors, heat & current drive components, diagnostics, etc.

- How large the TBR should actually be during the lifetime of the FPP is depending on the dynamics of the entire fuel cycle for the D-T plant. It accounts for:
 - **possible losses of tritium** in the different parts of the process and tritium trapping in the materials
 - reduction of breeding in the time with the Li burn-up
 - duplication time (time necessary to produce the tritium amount necessary to start a new FPP)
 - storage capabilities
 - natural decay of tritium (half-life of 12.3 y)
 - safety inventory limits

U. Fisher et al, (2015) Neutronics requirements for a DEMO fusion power plant, FED 98–99, 2134–2137

Current BB design variants: the HCPB concept

Helium Cooled Pebble Bed Concept (HCPB)

- Structural Material: EUROFER (RAFM steel), ~3000 t
- Breeder: KALOS (Li_4SiO_4 + 35 mol% Li_2TiO_3) in form of a pebble bed, ⁶Li at 60%, ~165 t
- Neutron multiplier: Beryllide (TiBe₁₂) hexagonal rods, 612 t
- Coolant: helium 300-520°C @ 8 MPa, ~ 4.2 t

G. Zhou et al, (2023) The European DEMO Helium Cooled Pebble Bed Breeding Blanket: Design Status at the Conclusion of the Pre-Concept Design Phase, Energies, 16, 5377, DOI: 10.3390/en16145377

DB outlet



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Purge gas

Current BB design variants: the WCLL concept

Water Cooled Lead Lithium Concept (WCLL)

- Structural Material: EUROFER (RAFM steel), ~3500 t
- Breeder/neutron multiplier: PbLi (⁶Li at 90%) liquid (~330 °C @ 0.25-1.55 MPa), ~10,000 t,
- Coolant: Water (295-328°C @ 15.5 MPa), ~520 t
- Plasma protection: 2 mm W layer (wo Limiters)
- T extraction from recirculating PbLi

Identified risks as of end pre-CD phase:

	Risk ID	Risk
	.001	Low reliability of BB system
	.002	Low efficiency of PbLi draining
	.003	FW based on thin EUROFER + W-armor
	.005	Low tritium breeding performance
	.006	Large amount of transmutation helium in PbLi
	.010	Large T permeation to coolant
	.012	WCLL operating with EUROFER temp. irradiated <400 °C (DBTT shift)
	.013	Pressure transient uncertainties due to PbLi-water interaction
	.022	Diffusion of Li into anti-permeation barriers and production of T + He there



Motivation for water-cooled BB Alternative variants

Motivation:



- Poloidal water tube distribution:
 - Poloidal tubes:
 - (1) Less tubes, less welds, **↑ reliability**
 - (2) Less tubes, less surface, **V T**-permeation
 - (3) Less tubes, less water, more PbLi, **↑ TBR**
 - (4) Easier draining
 - BB similar to HX/SG =>
 TRL/RoX
 - Segments split in several poloidal regions
 - Limit heat flux per tube
 - Allows systems integration (H/CD, limiters...)
 w/o splitting segments
- "Double bundle" of simple tubes
 - 3-chamber idea of S&T HX (K.-H. Funke)
 - (5) Intermediate chamber between PbLi and water to avoid contact in case of internal LOCA
 - (6) 3rd chamber filled with He gas: used to remove permeated T before it reaches water



3450

al. (1995)

Giancarli et

BLANKET

TOP-DIVERTO

"3rd chamber"

PbLi inflow

"3rd chamber"

PbLi outflow

INBOARD

) Exploring variants: WCLL Double bundle



Exploring variants: Water-cooled Lead Ceramic-Breeder (WLCB)

- Background: a short story...
 - Idea started in **FP8**: HCPB issue with beryllium -> deep exploration of alternative n-multipliers -> Pb/Pb-alloy ۲
 - He-cooled molten Pb and ceramic breeder blanket: oral presentation at SOFT 2018 (FED-2019, FED-2019)
 - Curiosity for a water-cooled version -> WLCB, as radial CB pins (FED-2021, FED-2021)
- FP9: further work on a WLCB with poloidal configuration of advanced ceramic breeder (ACB) tubes and simpler cooling structures
- Seen as a best trade-off between HCPB and WCLL:
 - To avoid current issues in HCPB with shielding, multiplier technology and costs
 - To mitigate issues with T-permeation and avoid T-extraction risks from PbLi in WCLL variants
 - To avoid use of anti-permeation barriers in BB (TBC)
 - To use proven water PWR tech



Good TBR in compact space

- Proven water PWR tech
- More mature PHTS/BoP

F. A. Hernandez et al, (2023) Alternative water-cooled BB concepts for the EU DEMO: Overview on studies and perspectives, Presentation @ISFNT-15, Las Palmas

Exploring variants: Water-cooled Lead Ceramic-Breeder (WLCB)

- Structural Material: EUROFER (RAFM steel)
- Coolant: Water at PWR conditions (285-325 °C @155 bar)
 - cooling scheme: BZ and FW in series
 - radial cooling plates (acting as stiffeners)
- Breeder: ACB (Li₄SiO₄ + 35 mol% Li₂TiO₃) in form of a pebble bed, ⁶Li at 60% and Li₈XO₆, X=Pb, Zr...) in cassettes
- Purge gas: He + %H2 @2bar
- Neutron multiplier: molten Pb in cassettes
- Neutron spectra shifter: metal hydride such as ZrH_x (?) or YH_x (?) in cassettes
- Cassettes (cladding): SiC (?) ~2 mm thick





Breeding Blanket Qualification Strategy: the general approach



M.A. Abdou et al. (2015) Blanket/first wall challenges and required R&D on the pathway to DEMO, FED 100, 2-43, DOI: 10.1016/j.fusengdes.2015.07.021



Current EU-TBM Programme

Water Cooled Lead Lithium Concept (WCLL) - TBM

- The **FW** actively cooled with 7 x 7 mm² square channels
- **Double Wall Tubes (DWT)** with Øi 8 mm kept for DEMO relevancy
- **Coolant** water at @15.5 MPa, 295-328 °C
- Recirculating PbLi @0.2-1 kg/s .
- GLC technology for tritium extraction from PbLi







tion at Stiffening

BU PbLi inlet/ou

Helium Cooled Ceramic Pebble (HCCP) - TBM

- The FW actively cooled with 15x15 mm² square channels. ٠
- Breeder: Li₄SiO₄ in pebbles beds •
- Neutron multiplier: Be in pebble beds •
- Coolant: He at 8 MPa, 300-500 °C inlet/outlet temperature •
- Power extraction through curved cooling plates •
- Purge gas for T extraction: He + H_2 @0.2-0.4 MPa •









A VNS for the nuclear qualification of Breeding Blanket concepts

R = 2.53m, B ₀ = 5.4 T		
A=4.6	High aspect ratio to create space on the inboard side while minimising the surface	
CS	Nb ₃ Sn, sized to ramp up the plasma, $I_p = 1.76$ MA	
TF coil	Nb ₃ Sn or HTS, B _{max} =12.8 T – trading-off B with TFC size	
P _{fus} / P _{aux}	29 MW / 42 + 10 MA	



Testing options and testing approach in the VNS









